

Hydrogen as aviation fuel - Workshop 2023 Aircraft Certification Fire and Explosion challenges

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H2 Challenges





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Hydrogen, a new substance on board

- → With the need and wish for more sustainable flying, Hydrogen is considered to be a very promising candidate:
 - \rightarrow Either as reactant in a Fuel Cell System
 - \rightarrow Or as a combustive fuel an engine









Hydrogen, a new substance on board

- → Hydrogen (H2) has specific hazards, with own characteristics.
- → Predominant (mostly feared) are fire or explosion.

\rightarrow Others include:

- → Mechanical/material hazards (i.e. embrittlement, or failure storage systems)
- → Crashworthiness
- → Physiological hazards
- \rightarrow Cryogenic (for the use of Liquid H2 (LH2))
- \rightarrow Fueling and handling hazards



Different possible utilisations of H₂ foreseen

→ As reactant in a fuel cell, generating electrical power for, i.e.:

- \rightarrow Energy for Propulsion
- → Aircraft Galley Power Trolley Cart
- → Emergency Power (e.g. replace main battery, RAT)
- → Stand Alone Power:
 - \rightarrow Medical evacuation
 - → Electronic warfare
 - → Maritime surveillance
- → Auxiliary Power System
- \rightarrow As combustion fuel in stead of jet fuel.









Storage and distribution

- Pure Hydrogen:
- \rightarrow Liquid
- → Gaseous

Examples of other storage possibilities:

- → Hydrocarbons (reforming)
- → Solids (Metal Hydrides, on surfaces, etc)
- \rightarrow Water (electrolyse) H₂



ndothermic : Heating between 55°

to 200°C depending on the meta





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Liquid H2 storage

Liquid storage

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- \rightarrow H₂ is liquid T<20°K (-253°C), cryogenic
- \rightarrow At ca. 1 bar 5 kg H₂ is stored in 75 litre tank

→ Currently used in space propulsion





Liquid H2 storage

- \rightarrow Liquid storage is a mature solution
- → Relatively low pressures (<12 bar)
- \rightarrow Liquefying H₂ requires:
 - \rightarrow very pure H₂
 - → ortho to para conversion (@20K 99% para)
- → Expensive both in costs and energy





Gaseous H2 storage

→ Different pressure vessel types, III and IV light weight and high pressure vessel





Gaseous H2 storage

Compressed gaseous

- \rightarrow At 700 bar, density of H₂ is 42 kg/m³: 5 kg H₂ fits in 125 litre tank
- → Cars use this technology, giving a range of 600 km







H2 Turbofan/Turbopropeller

→ H2 can directly feed turbofan/turbopropeller engine combustion chamber





Fire and explosion risks

Hydrogen Combustion

- \rightarrow 3 elements needed
- \rightarrow Auto-ignition T: 538 °C
- → Wide flammability range vs concentration

Combustion Hazards

Fire

Triangle

FUEL

Hydrogen

Air

Oxygen

Heat Eletric Arc

Electric Spark

 \rightarrow Low ignition energy

90

80

70

60

50

40

30

20

10

0







Fire and explosion risks

→ Hydrogen flame is pale blue
 → Adiabatic flame T:
 → H2/Air -> 2045 °C
 → H2/O2 -> 3200 °C



→ Little infrared heat, but substantial ultraviolet radiation:
 → Even close, only little sensation of heat for a human being



Hazards summary

\rightarrow H2 fire and explosion hazards:

- \rightarrow H2 ignition
- \rightarrow H2 combustion
- \rightarrow H2 fires: microflames, H2 deflagration, H2 detonation
- → Flammable mixture ignition:
 - \rightarrow Due to electrical sources
 - \rightarrow Due to mechanical sources
 - \rightarrow Due to thermal sources
 - \rightarrow Resonance ignition
 - \rightarrow Flammability limits

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H2 Fire/Explosion Challenges





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Product Safety Objectives

- \rightarrow Example for assessing (CS-25) regulatory impacts:
 - → Maintain the same level of safety achieved by circa 70 years of fire/explosion regulatory evolutions for large airplane commercial transport: H2 presence shall not degrade this achieved level.
 - \rightarrow Keep the spirit of CS-25 Fire & Explosion Safety requirements that are:
 - → **PRESCRIPTIVE and DESIGN ROBUSTNESS** oriented
 - → **NUMEROUS**: in all CS-25 subparts with:
 - → **GENERAL rules** (i.e CS 25.1309 CCA with FESRA PRA's, minimization with CS 25.863,...)
 - → SPECIFIC rules :DFZ adjacent zone with 25.1182, Tank Safety with CS 25.981/954, Designated Fire Zones with CS 25.1181/25J1181, Crashworthiness with CS 25.963/25.993/25.994, Occupant protection from external fire with CS 25.856,...
 - → MULTI-LAYERS rules Supplementing : CS 25.981 over CS 25.1309 Overlapping: Requirement for DFZ, FFLZ, FZ ...



- → Zone Concept Issue : H2 presence on-board aircraft is impacting existing fire/explosion requirements and already defined fire/explosion risk zoning. Possible new concept to address specificities.
 - → Impact onto Designated Fire Zone (DFZ), Flammable fluid Leakage Zone (FFLZ), Fire Zone (FZ), zone adjacent to DFZ (xx.1182), 2D-Nacelle, ...
 - → Impact on Fuel Tank Safety (FTS) perimeter applicability:
 - \rightarrow H2 distribution is likely to be treated as an H2 tank is to be treated
 - → A flammable fluid leak is supposed to be a failure condition not a nominal condition (porosity). Strategy to be defined but likely to be treated under fuel tank safety rather than an FFLZ (leak is a failure).
 - → New zone for electrical fire threat : Electrical Fire Withstanding Zone (EFWZ)
 - → New zone for fuel cell fire threat : Fuel Cell Fire Withstanding Zone (FCFWZ)



\rightarrow H2 Fire Extinguishing

- → Issue : Potential loss of one fire layer of protection with no (H2) performant fire extinguishing agent/system
 - → Today CS-25 requires 2 shots capability
- \rightarrow Do not imply that fire extinguishing agent/system will not be necessary
 - → Presence of other flammable fluids (oil, hydraulics)
 - \rightarrow Residual burning from H2 fire exposure
- → Is reliance placed on H2 supply shutting off sufficiently balancing the loss of that fire protection layer?



→ H2 Fuel Tank Safety

→ Issue : CS 25.981 is a 2 layers, self sustained rule concept

- \rightarrow The intent of the 2 layers probably need to be redistributed
- → Whereas there was some different treatment between classic fuel distribution and classic fuel storage (ullage presence) : it may no longer be true for H2 distribution/storage
- \rightarrow Inversed concept:

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CS 25.981	Classic Fuel Tank	H2 Tank + Distrib.
Prevention	Ignition source prevention with low probability	Minimize ignition risk
Minimization	Minimized exposure to flammability range	Prevent exposure to flammability range with low probability

\rightarrow H2 Explosion

- → Fuel Tank Safety: Is a tank explosion "containment" and Continued Safe Flight and Landing (CSFL) path still an option?
- → General : Is it one explosion problematic or 2 problematics with deflagration and detonation to be addressed?
 - \rightarrow Possibly a design robustness intent for deflagration
 - → Possibly a minimum design features and a low probability approach for detonation
 - \rightarrow Will have to play on prevention from moving from deflagration to detonation



- → H2 Combustor Burnthrough
 - → CS-2x makes some assumptions that a flame can exit the turbine engine combustion chamber (CS 2x.903)
 - Parallel with combustor burn through flame (25.903, British Standards Institution Specification 3G100: Part 2: Section 3: Sub-section 3.13, dated December 1973/ AC 20-135)
 - Flame: 3min, 1700°C (3000°F), 350-550 psi, 1-inch diameter.
 - \rightarrow Issue :
 - \rightarrow What sort of H2 flame to deal with?
 - \rightarrow How do we come to a standard?

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- \rightarrow H2 Fire in a powerplant environment
 - \rightarrow CS-Definition
 - → Assumes:
 - \rightarrow A temperature
 - \rightarrow A heat flux
 - → 2 time durations
 - → Recognizes:
 - \rightarrow Steel (Titanium) and Aluminum material equivalency to fire exposure duration
 - \rightarrow Issue :
 - → Need to understand how those assumptions could be invalidated with H2 and what could be the new one
 - → <u>Note</u>: that notion of fire size does not exist, neither distance at which the fire is standardized: does it need to be defined in the context of H2?
 - → <u>Note:</u> H2 Fire presence duration is a minimum of 5min (based on crew reaction same assumption as for classics fuel installation). Plus a certain duration to be determined for fire presence after crew reaction/procedure intitiation.



- → H2 Fire in a powerplant environment: getting a standard
- \rightarrow How was it done for ISO2685/AC 20-135 ?
 - ▶ Historic Genesis of ISO2685 / AC 20-135 for Powerplant (jet fuel) Fire Testing
 - > In summary:
 - Prompted by in-service issues with an urgent need for a fire test program. (1939)
 - DC-3 Pratt & Whitney 1830-B (Wasp) from 1939 to 1941.
 - Curtiss Wright CW-20 installation with the engine and Waco YKS-37. Ending around 1943
 - Lot of full scale testing
 - Progress with time

	Organization / Time Frame	Development Test Reports	Powerplant Regulations	
	CAA; 1939 to 1950s	 Engine/nacelle fire tests TD No. 31 & No. 33, 1943 Various other test reports 	 CARs 4 (aircraft) & 13 (engine), 1946 SRR No. 259, 1947 	
	FAA; 1960s-1980s	 Power plant Installation fire tests (NA-69-26, 1969) Oil burner Reevaluation (RD-76-213, 1976) Various other test reports (Power plant Report 3A, etc) 	 SRR No. 453, 1961 FAR regulations AC 20-135 Draft (1988) 	
3	FAA; 1990 to current	 Next Gen burner test reports (various) Propane vs kerosene comparison test reports (various) 	 14 CFR regulations AC 20-135 (1990) AC 33.17-1 (2002); 33.17-1A (2009) AC 20-135 Change 1 (2018) 	



- → H2 Fire in a powerplant environment: getting a standard
- \rightarrow How to do it?
 - Will not wait in-service issues
 - Full scale testing is part of the process
 - Progress with time
- → Could be a progression from basics understanding and characterization supplemented with data from project blocks and dedicated standard testing activities, all with support of modelling.



→ H2 Fire in a powerplant environment: getting a standard



BASICS \succ

H2 flame	H2 flame duration	H2 material withstanding capability	
Litterature Review	Litterature Review	Litterature Review	
Testing - BASICS Flame - Free H2 Flow - Explore Measure - Temperature - Temperature - Heat Flux - Size vs f(flow) - T mapping (x,y,z) - HF mapping (x,y,z) Repeatibility	Assumptions - Analysis - BASICS f(trapped volume, leak rate)	Testing - BASICS Coupons testing - Sheets - Tubes Different Material - Aviation - Steel - Titanium - Aluminum - Composite, Elastomeric Thickness - Standard (vs known FR/FP) - Explore (till 5min / 15min) Measure - Melting duration - Burnthrough duration - Skin temperature	Flame-to-specimen distance Testing - BASICS Distance - Standard (vs known fire testing conditions) - Explore Repeatability
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PROJECT BLOCK			
H2 Leak	H2 flame	H2 flame duration	H2 material withstanding capability
Failure Combination Assumptions	Full Scale Testing (design dependent)	Full Scale Testing (design dependent).	Full Scale Testing (design dependent)
FMEA (design dependent)	Flame - Free	 f(trapped volume, leak rate) from design and leak 	TC design Measure
 Leak Characterization Defect database From FMEA Simulated defects Defect variation 	 Closed H2 Flow From Leak Characterization Measure Temperature 	characterization. Measure - Flame duration - T = f(t) - Hazardous quantity	 Melting duration Burnthrough duration Skin temperature
Measure - Leak rate: f(defect, flow conditions)	 Heat Flux Size vs f(flow) T mapping (x,y,z) 		Flame-to-specimen distance Full Scale Testing (design
ZEASA	- HF mapping (x,y,z)		dependent Distance - From design

STANDARD



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In-flight fires: zonal analysis

 \rightarrow H2 leak in pressurized areas:

- \rightarrow increased risk of explosions
- → even concentrations of hydrogen below the lower flammability limit could adversely affect the flammability performance of materials and constructions
- → higher level of severity of the fire threats in critical zones: inaccessible areas, cargo compartments, but also in occupied areas
- \rightarrow Mitigating measures:
 - → Prevent leakage from hydrogen systems to other non-powerplant zones
 - \rightarrow Ventilation / detection / isolation



Post Crash fire

- → When using Hydrogen as fuel, the fire hazard resulting from a Hydrogen leak after a crash may be very different compared to that resulting from traditional types of fuel, due to the Hydrogen phenomenology:
 - \rightarrow LH2 "instantaneous" evaporation upon leaking
 - \rightarrow LH2 interaction with Air
 - \rightarrow Gaseous H2 lighter than air
 - → H2 ignition can lead to Jet flame or explosion (deflagration / detonation)
 - \rightarrow H2 Bleve risk (inside the tank)
 - ightarrow H2 flame is barely visible

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Post Crash fire

→ Need to reconsider flammability standards:

- → Burnthrough protection achieved through CS 25.856(b) may be inadequate: new performance based requirements need to be specified
- → Meeting current certification specifications (e.g. for Large Aeroplanes CS 25.853 and CS-25 App. F Parts II, IV and V) may not be sufficient to maintain survivable conditions in the cabin until safe evacuation is achieved.
- → Minimum performance standards for flammability of materials used in the construction of escape slides (ref. ETSO-C69c and Chapter 9 of Aircraft Materials Fire Test Handbook) may not be adequate to withstand a hydrogen fire.



Post Crash fire

→ CS 25.803(a):

Each crew and passenger area must have emergency means to allow rapid evacuation in crash landings, with the landing gear extended as well as with the landing gear retracted, considering the possibility of the aeroplane being on fire.



Post Crash fire

- → Before launching the emergency evacuation, the crew should have a means to detect the presence of a fire that may affect evacuation from the aircraft: it should be possible to identify a hydrogen fire in any light condition.
- → The location and the level of performance of the available emergency exits, as well as the design and performance of the associated egress assist means, should ensure that evacuees are not directed towards areas inside the cabin or on the ground with risk of lethal injury due to H2 hazard.



Post Crash fire

It may be necessary to replace existing CS-25 requirements and/or, whenever appropriate, to introduce special conditions.

→ CS 25.807(e):

Emergency exits must be distributed as uniformly as practical, taking into account passenger seat distribution.

→ CS 25.807(f)(3):

If more than one floor-level exit per side is prescribed, and the aeroplane does not have a combination cargo and passenger configuration, at least one floor-level exit must be located on each side near each end of the cabin.



Post Crash fire

- → Depending on the design of the aircraft, it may be preferrable to concentrate exits in areas that minimize exposure to any hazards generated by the hydrogen systems installation.
- → Evacuees should be directed to safe areas after reaching the ground, at sufficient distance from the aircraft to mitigate the risk of exposure to explosions.



Definition of **Hazard areas** following a similar approach as already proposed by EASA for VTOL aircraft (ref. MOC-2 SC-VTOL Issue 3):

Hazard areas: Areas around the aircraft where a hazard to persons or equipment may exist, for example due to moving surfaces, engine exhaust or battery venting in case of fire, should be identified and depicted in the AFM. Corresponding hazard markings should be present on the aircraft.







→ Certainly not exhaustive list of problematics ... → Batteries fire/explosion risk...

→ Looking forward to the discussion:

- \rightarrow Any missing problematics,
- \rightarrow priority,
- → working groups initiation...





Thank you!

Please share proposals/concerns:

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